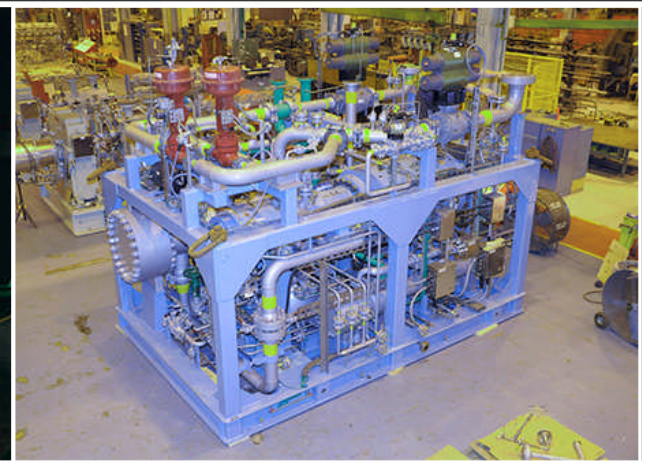


**DRESSER-RAND®**

Equipment life-cycle, challenges for sour  
service in Oil & Gas handling →  
IICHe (NRC) New Delhi

**Vinod Bhatt**



**May 2<sup>nd</sup> 2015**

Bringing energy and the environment into harmony.®

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The Private Securities Litigation Reform Act of 1995 provides a “safe harbor” for certain forward-looking statements so long as such information is identified as forward-looking and is accompanied by meaningful cautionary statements identifying important factors that could cause actual results to differ materially from those projected in the information.

The use of words such as “may”, “might”, “will”, “should”, “expect”, “plan”, “outlook”, “anticipate”, “believe”, “estimate”, “appear”, “project”, “intend”, “future”, “potential” or “continue”, and other similar expressions are intended to identify forward-looking statements.

All of these forward-looking statements are based on estimates and assumptions by our management that, although we believe to be reasonable, are inherently uncertain. Forward-looking statements involve risks and uncertainties, including, but not limited to, economic, competitive, governmental and technological factors outside of our control, that may cause our business, industry, strategy or actual results to differ materially from the forward-looking statements.

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# Safety Moment

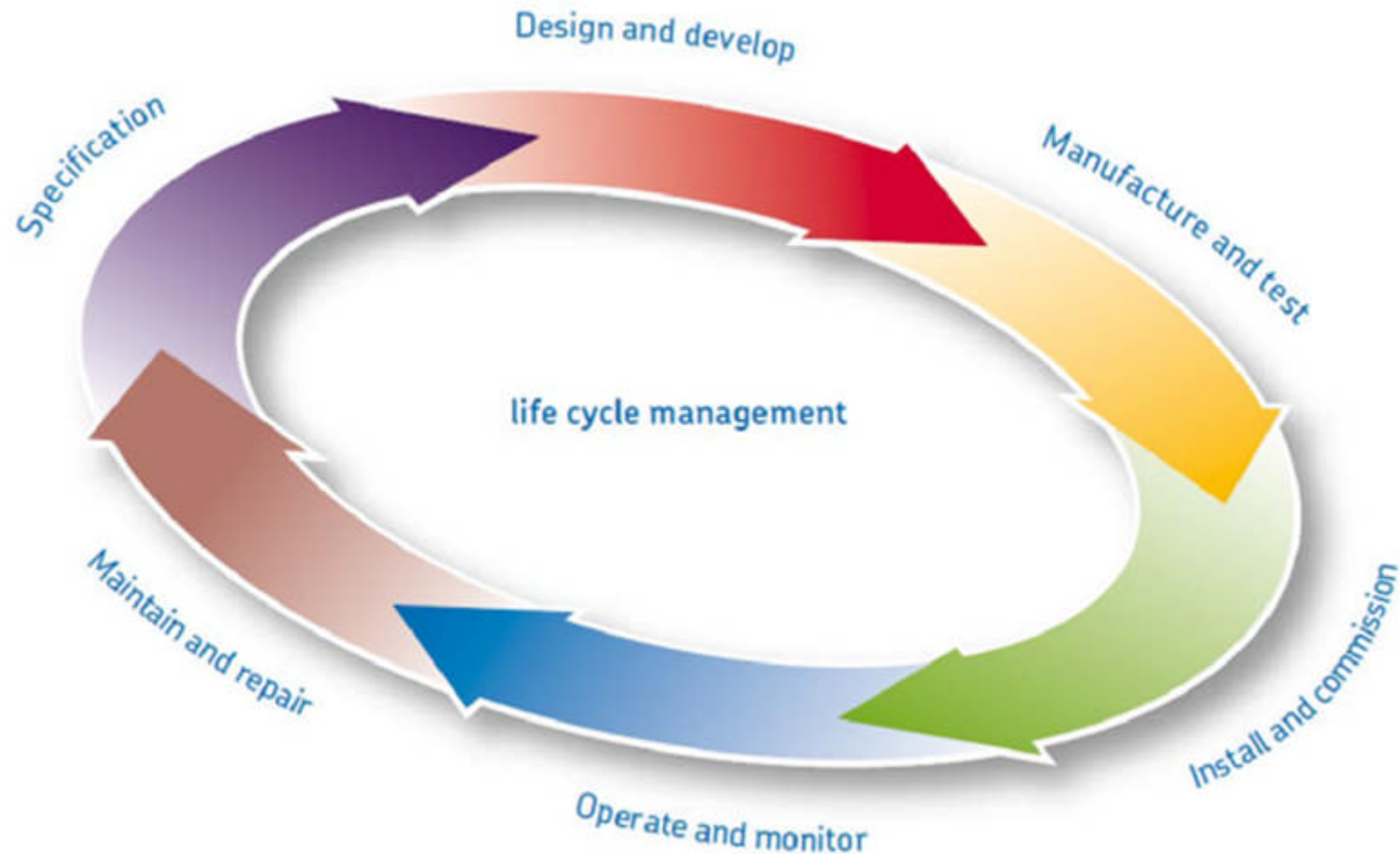


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# Agenda

- Safety moment
- Equipment Life cycle
- Sour Service
- Case study Sour Gas mix
- HIRI wisdom

# Life Cycle Management



# Life Cycle Management

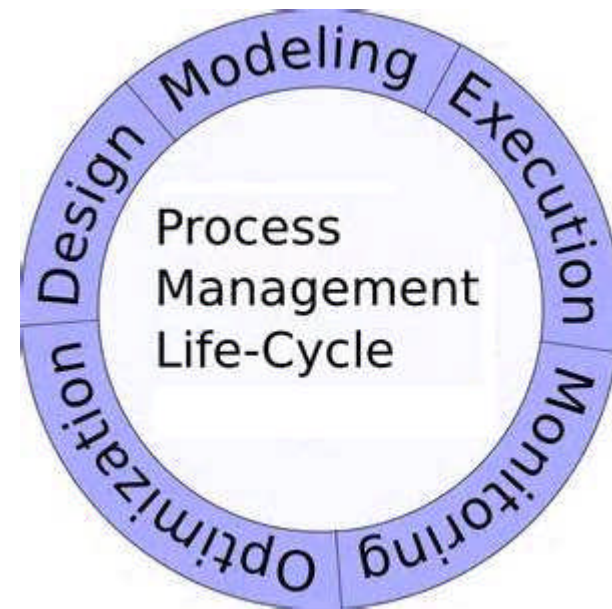
Contd.

- Freezing process specification, selection and design of equipment.
- Design adequacy checks & performing optimization.
- Material selection-Compliance to specifications.
- Necessary simulations suiting site & Licensor recommendation.
- Adequate instrumentation & controls-current technology.

# Life Cycle Management

Contd.

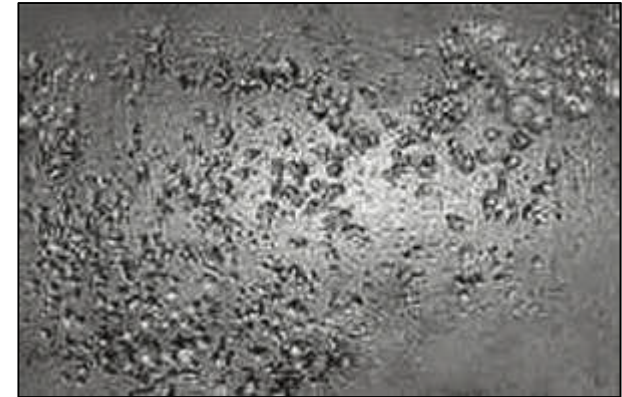
- Quality controls and testing with up to date methods.
- Predictive and preventive maintenance plans-Stocking-Conditioning monitoring.
- Setting trends-continuous review-update all above.



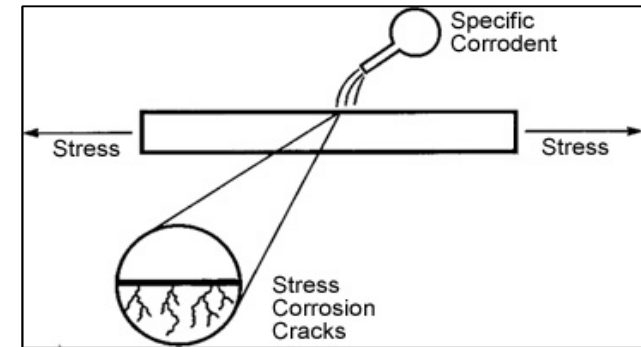


# Corrosion in Sour Environment

- Presence of sulfide in chemical mix and SOUR environment causes major threat on life cycle. The result is corrosion.
- While handling oil & gas(refining process), such as pitting corrosion(water droplets), embrittlement from H<sub>2</sub> & stress corrosion cracking(sulfides).
- From a materials standpoints, carbon steel is used for upwards of 80% of equipment components, which is beneficial due to its low cost and availability.



Pitting corrosion



Stress corrosion



# Corrosion in Sour Environment

- Common replacement materials are low alloy steels with Chromium & Molybdenum with Stainless steel.
- Now a days Nickel, Titanium, Copper, Duplex SS & Super duplex are widely used.
- Material selection has to be optimistic considering the most problematic areas as also the economic optimal use.
- Corrosion has to be tackled by complex system of monitoring, preventive repairs and careful use of materials.



Gas cylinder corrosion

## Review of Coolers (AES type) for H<sub>2</sub>S (51.31 mole %) & MeSH (47.95 mole %) service

3-stage Reciprocating gas compressor

Having Gas MW: 40.75

Service	Intercooler 1	Intercooler 2
Gas inlet T °C	114	121
Gas discharge T °C	60	90
Gas Operating Pressure BARG	8.527	18.986
Cooling water inlet T °C	33	33
Cooling water outlet T °C	40.3	37.2

# P-T Dew point table

POINT #	VAP FRAC	PRES bar a	TEMP °C
1	1	3.0	19.0
2	1	3.4	22.7
3	1	3.9	26.1
4	1	4.3	29.2
5	1	4.7	32.1
6	1	5.2	34.8
7	1	5.6	37.3
8	1	6.0	39.7
9	1	6.4	42.0
10	1	6.9	44.1
11	1	7.3	46.1
12	1	7.7	48.1
13	1	8.2	49.9
14	1	8.6	51.7
15	1	9.0	53.5
16	1	9.5	55.1
17	1	9.9	56.7
18	1	10.3	58.3
19	1	10.7	59.8
20	1	11.2	61.3
21	1	11.6	62.7
22	1	12.0	64.1
23	1	12.5	65.4
24	1	12.9	66.7
25	1	13.3	68.0
26	1	13.8	69.2
27	1	14.2	70.4
28	1	14.6	71.6
29	1	15.1	72.8
30	1	15.5	73.9
31	1	15.9	75.0
32	1	16.3	76.1

POINT #	VAP FRAC	PRES bar a	TEMP °C
33	1	16.8	77.1
34	1	17.2	78.2
35	1	17.6	79.2
36	1	18.1	80.2
37	1	18.5	81.2
38	1	18.9	82.2
39	1	19.4	83.1
40	1	19.8	84.1
41	1	20.2	85.0
42	1	20.6	85.9
43	1	21.1	86.8
44	1	21.5	87.6
45	1	21.9	88.5
46	1	22.4	89.3
47	1	22.8	90.2
48	1	23.2	91.0
49	1	23.7	91.8
50	1	24.1	92.6
51	1	24.5	93.4
52	1	24.9	94.2
53	1	25.4	94.9
54	1	25.8	95.7
55	1	26.2	96.4
56	1	26.7	97.2
57	1	27.1	97.9
58	1	27.5	98.6
59	1	28.0	99.3
60	1	28.4	100.0
61	1	28.8	100.7
62	1	29.3	101.4
63	1	29.7	102.1
64	1	30.1	102.7

Contd.

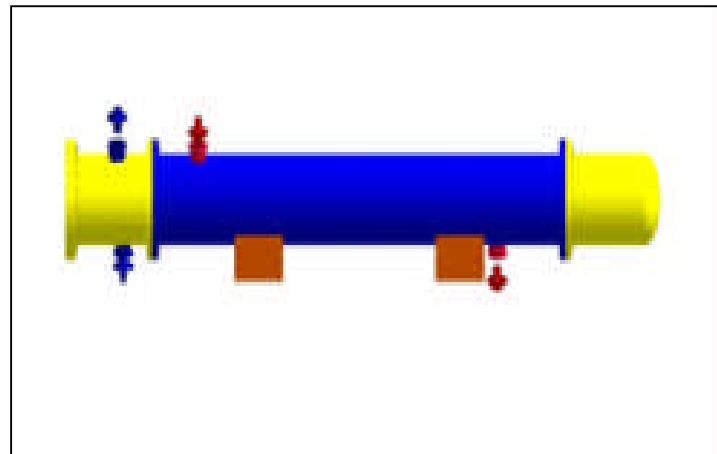
POINT #	VAP FRAC	PRES bar a	TEMP °C
65	1	30.5	103.4
66	1	31.0	104.1
67	1	31.4	104.7
68	1	31.8	105.3
69	1	32.3	106.0
70	1	32.7	106.6
71	1	33.1	107.2
72	1	33.6	107.8
73	1	34.0	108.4
74	1	34.4	109.0
75	1	34.8	109.6
76	1	35.3	110.2
77	1	35.7	110.8
78	1	36.1	111.4
79	1	36.6	111.9
80	1	37.0	112.5

SHEET 4 OF 9

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## Review of Coolers (AES type) for H<sub>2</sub>S (51.31 mole %) & MeSH (47.95 mole %) service Contd.

- Coolers IC1 & IC2 designed using HTRI which showed following results.
- It gave weight fraction vapour at outlet of coolers as 1 that means no liquid in the outlet stream.
- Reviewing the reports in detail, it showed local weight fraction vapour as 1.



12

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# HTRI wisdom



- At site during actual run, condensation was noticed in both the coolers.
- Referred to HTRI Technical support. HTRI stated:
  - ❑ If the dew point of gas is @ 55 °C then condensation may take place if the skin temperature on that side falls below that temperature.
  - ❑ Looking at final HTRI run min. skin temperature = 44.1 °C & max. skin temperature = 56.9 °C

# HTRI wisdom

Contd.

- ❑ HTRI therefore feels that site will definitely get some condensation on the surface of the fouling layer.
- ❑ However gas/ fluid temp at exit from exchanger is above the dew point
- ❑ Thus any condensation will re-evaporate into the vapour phase (assuming its in contact with vapour and does not drain to the bottom of the shell and collect there).

# HTRI response

Contd.

- In conclusion HTRI statement assumes that calculated dew point is correct.
- If it is wrong then, depending on the dew point one may or may not get condensation taking place.
- HTRI also suggested to re- verify actual gas mix, properties and dew point at site.

Xist Ver. 6 SP3 21-03-2013 11:06 SN: 1500214814

Barg Units

TUBE LAYOUT, BAFFLE CUT, SEAL ROD DIA CHANGED

INTERCOOLER1

Rating - Horizontal Multipass Flow TEMA AES Shell With Single-Segmental Baffles

**No Data Check Messages.**
**See Runtime Message Report for Informative Messages.**

Process Conditions		Hot Shellside		Cold Tubeside	
Fluid name			GAS		COOLING WATER
Flow rate	(1000-kg/hr)		2.8340		5.8500
Inlet/Outlet Y	(Wt. frac vap.)	1.0000	1.0000	0.0000	0.0000
Inlet/Outlet T	(Deg C)	114.00	60.00	33.00	40.30
Inlet P/Avg	(barG)	8.527	8.496	4.000	3.926
dP/Allow.	(bar)	0.061	0.088	0.147	0.343
Fouling	(m2-K/W)		0.000258		0.000344
Exchanger Performance					
Shell h	(W/m2-K)	416.90	Actual U	(W/m2-K)	293.01
Tube h	(W/m2-K)	5421.3	Required U	(W/m2-K)	290.32
Hot regime	(--)	Sens. Gas	Duty	(kcal/hr)	42639.
Cold regime	(--)	Sens. Liquid	Eff. area	(m2)	3.800
EMTD	(Deg C)	44.9	Overdesign	(%)	0.93
Shell Geometry			Baffle Geometry		
TEMA type	(--)	AES	Baffle type		Single-Seg.
Shell ID	(mm)	254.10	Baffle cut	(Pct Dia.)	36.5
Series	(--)	1	Baffle orientation	(--)	Perpend.
Parallel	(--)	1	Central spacing	(mm)	154.85
Orientation	(deg)	0.00	Crosspasses	(--)	9
Tube Geometry			Nozzles		
Tube type	(--)	Plain	Shell inlet	(mm)	102.26
Tube OD	(mm)	19.050	Shell outlet	(mm)	102.26
Length	(mm)	2200.	Inlet height	(mm)	44.700
Pitch ratio	(--)	1.3333	Outlet height	(mm)	44.700
Layout	(deg)	90	Tube inlet	(mm)	42.850
Tubecount	(--)	32	Tube outlet	(mm)	42.850
Tube Pass	(--)	4			
Thermal Resistance, %		Velocities, m/s		Flow Fractions	
Shell	70.28	Min	Max	A	0.027
Tube	6.54	—	—	B	0.485
Fouling	19.76	Crossflow	—	C	0.285
Metal	3.42	Window	—	E	0.071
				F	0.131





## Output Summary

Released to the following HTRI Member Company:  
DRESS RAND INDIA PVT.LTD  
DRESS RAND INDIA PVT.LTD

Page 1

Xist Ver. 6 SP3 21-03-2013 11:19 SN: 1500214814

Barg Units

### INTERCOOLER2

Rating - Horizontal Multipass Flow TEMA AES Shell With Single-Segmental Baffles

1 No Data Check Messages.

2 See Runtime Message Report for Warning Messages.

Process Conditions		Hot Shellside		Cold Tubeside	
Fluid name		GAS		COOLING WATER	
Flow rate	(1000-kg/hr)		2.8340		6.3490
Inlet/Outlet Y	(Wt. frac vap.)	1.0000	1.0000	0.0000	0.0000
Inlet/Outlet T	(Deg C)	121.00	90.00	33.00	37.22
Inlet P/Avg	(barG)	18.986	18.967	4.000	3.972
dP/Allow.	(bar)	0.038	0.206	0.056	0.343
Fouling	(m2-K/W)		0.000258		0.000344

Exchanger Performance					
Shell h	(W/m2-K)	730.98	Actual U	(W/m2-K)	418.55
Tube h	(W/m2-K)	5238.0	Required U	(W/m2-K)	413.40
Hot regime	(--)	Sens. Gas	Duty	(kcal/hr)	26732.
Cold regime	(--)	Sens. Liquid	Eff. area	(m2)	1.091
EMTD	(Deg C)	68.9	Overdesign	(%)	1.25

Shell Geometry			Baffle Geometry		
TEMA type	(--)	AES	Baffle type		Single-Seg.
Shell ID	(mm)	193.68	Baffle cut	(Pct Dia.)	33
Series	(--)	1	Baffle orientation	(--)	Perpend.
Parallel	(--)	1	Central spacing	(mm)	104.40
Orientation	(deg)	0.00	Crosspasses	(--)	5

Tube Geometry			Nozzles		
Tube type	(--)	Plain	Shell inlet	(mm)	73.660
Tube OD	(mm)	19.050	Shell outlet	(mm)	73.660
Length	(mm)	1219.	Inlet height	(mm)	42.388
Pitch ratio	(--)	1.3333	Outlet height	(mm)	42.388
Layout	(deg)	90	Tube inlet	(mm)	42.850
Tubecount	(--)	18	Tube outlet	(mm)	42.850
Tube Pass	(--)	2			

Thermal Resistance, %		Velocities, m/s			Flow Fractions	
Shell	57.26		Min	Max	A	0.039
Tube	9.67	Tubeside	--	--	B	0.597
Fouling	28.23	Crossflow	--	--	C	0.219
Metal	4.85	Window	--	--	E	0.144
					F	0.000

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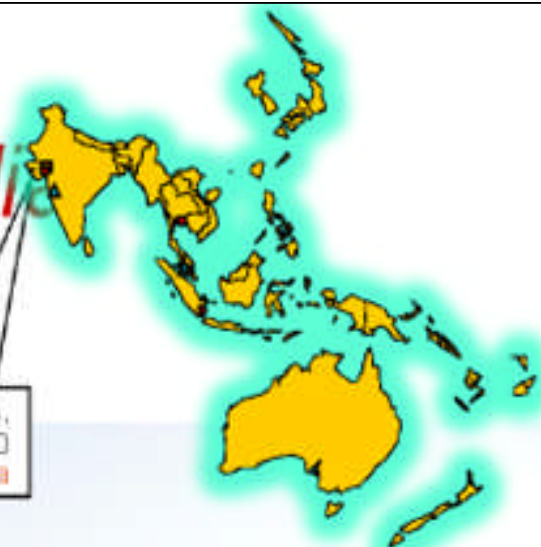




# Dresser-Rand, Naroda-India



NARODA,  
DAHMEDA ROAD  
INDIA



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## Questions - ??



**Sincere Thanks to  
IICHe- HTRI and you all**





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